



## A self-adaptive IMEX splitting capturing the multi-scale waves of compressible low-velocity flows

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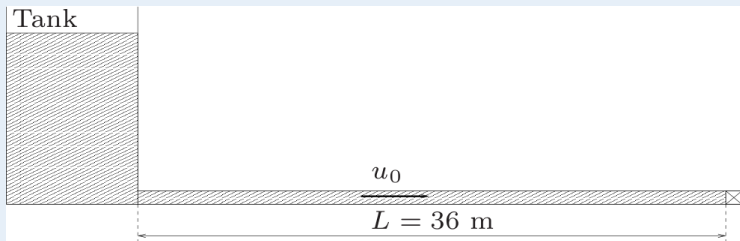
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- 1 Low-velocity flows endowed with a stiff equation of state
- 2 A dynamic Implicit-Explicit scheme
- 3 Numerical results

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# The Simpson's experiment : mechanical water hammer

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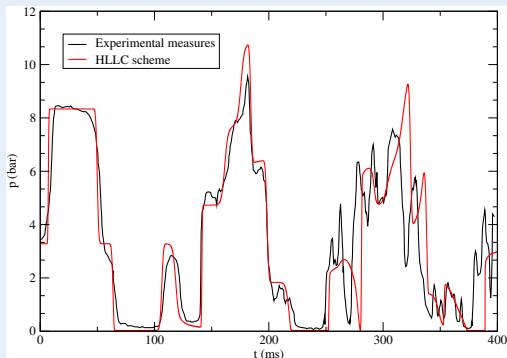


Simpson's set up

- Liquid water :  $p_0 = 3.281 \text{ bar}$ ,  $T_0 = 23.9 \text{ }^\circ\text{C}$ ,  $u_0 = 0.401 \text{ m}\cdot\text{s}^{-1}$ .
- At  $t = 0$  valve closure.
- Strong shock/rarefaction waves propagating up and down.

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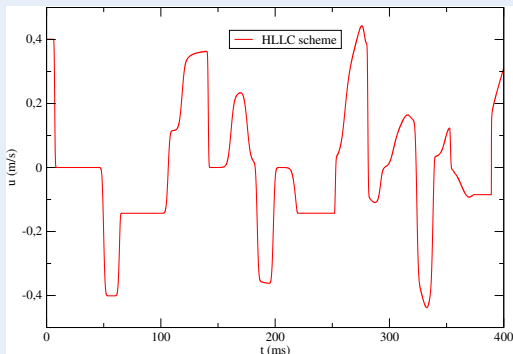


Time evolution of pressure :  $p(x = 27 \text{ m}, t)$

- $(p_{\max} - p_0) / p_0 \approx 1.93$ .

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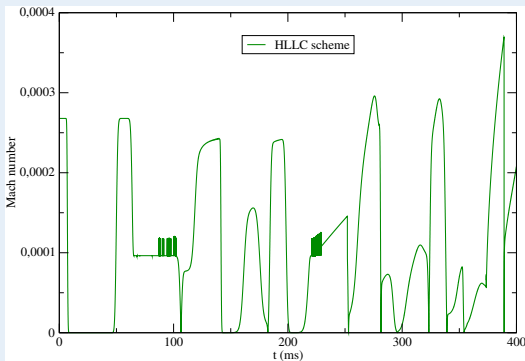


Time evolution of velocity :  $u(x = 27 \text{ m}, t)$

- $(p_{\max} - p_0) / p_0 \approx 1.93$ .
- $|u_{\max}| \approx 0.4 \text{ m}\cdot\text{s}^{-1}$ .

# The Simpson's experiment : mechanical water hammer

## Simpson's water hammer (Simpson, 1986, PhD)



Time evolution of the Mach number :  $M(x = 27 \text{ m}, t)$

- $(p_{\max} - p_0) / p_0 \approx 1.93$ .
- $|u_{\max}| \approx 0.4 \text{ m.s}^{-1}$ .
- $M_{\max} \approx 3.5 \times 10^{-4}$ .

Euler system with a passive tracer :

$$\begin{cases} \partial_t \rho + \partial_x (\rho u) & = 0, \\ \partial_t (\rho Y) + \partial_x (\rho Y u) & = 0, \\ \partial_t (\rho u) + \partial_x (\rho u^2 + p) & = 0, \\ \partial_t (\rho e) + \partial_x ((\rho e + p) u) & = 0. \end{cases} \quad \begin{cases} Y : \text{passive tracer,} \\ e = \frac{|u|^2}{2} + \varepsilon, \\ \varepsilon = \varepsilon^{EOS}(\rho, p). \end{cases}$$

Stiffened gas equation of state :

$$\varepsilon^{EOS}(\rho, p) = \frac{p + \gamma P_\infty}{(\gamma - 1) \rho}$$



# Analytical solution : symmetric double shock waves

	Left state	Right state
$\rho$ ( $kg.m^{-3}$ )	$\rho_{0,L} = \rho_0 = 10^3$	$\rho_{0,R} = \rho_0$
$u$ ( $m.s^{-1}$ )	$u_{0,L} = u_0 = 1$	$u_{0,R} = -u_0$
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**Table:** Stiffened gas symmetric double shock initial conditions

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$$\frac{P^* - P_0}{P_0} = M_0 \gamma \left( \frac{\gamma + 1}{4} M_0 + \sqrt{1 + \frac{(\gamma + 1)^2}{16} M_0^2} \right).$$

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Analytical pressure jump :

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Ideal gas EOS :  $P_\infty = 0$

$p = P$ ,  $p_0 = P_0$ .

$$\frac{p^* - p_0}{p_0} = M_0 \times O(1) \text{ w.r.t } M_0.$$

$$\Rightarrow \lim_{M_0 \rightarrow 0} \frac{p^* - p_0}{p_0} = 0.$$

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Numerical Application :  $\gamma = 7.5$ ,

$$P_\infty = 3 \times 10^8 \text{ (Pa)}.$$

$$\Rightarrow c_0 \approx 1500 \text{ m.s}^{-1}, T_0 \approx 22^\circ \text{C}.$$

$$\Rightarrow M_0 \approx 7 \times 10^{-4}, \alpha = 10^3.$$

$$\Rightarrow (p^* - p_0) / p_0 \approx 5.26.$$



# Allievi's model & Joukowski's jump conditions

## Derivation of Allievi's model (Allievi, 1902)

### Hypothesis :

- Euler system with constant temperature  $T_0$  :  $p = p^{\text{EOS}}(\rho, T_0) = p_0^{\text{EOS}}(\rho)$ ,  
 $\rho = (p_0^{\text{EOS}})^{-1}(p) = \rho_0^{\text{EOS}}(p)$ ,  $1/c = \sqrt{(\rho_0^{\text{EOS}})'(p)}$ .

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$$\partial_t \rho + u \partial_x \rho + \rho \partial_x u = 0,$$

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 $c_0 \approx 1.5 \times 10^3 \text{ m.s}^{-1}$ ,  $p_0 = \rho_0 u_0 c_0 \approx 15 \text{ bar}$ ,  $(\rho_0 c_0^2 \approx 22500 \text{ bar}$ ,  
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- Unsteady compressible low Mach number flows :  
 $M_0 \ll 1 \Rightarrow \rho = \rho_0 + O(M_0)$ ,  $c = c_0 + O(M_0)$ .

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$$\text{Allievi's model : } \begin{cases} \frac{1}{c_0^2} \partial_t p + \rho_0 \partial_x u = 0, \\ \rho_0 \partial_t u + \partial_x p = 0. \end{cases}$$

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 $M_0 \ll 1 \Rightarrow \rho = \rho_0 + O(M_0)$ ,  $c = c_0 + O(M_0)$ .
- Eigenvalues and jump relations :  $\lambda_0^\pm = \pm c_0$ .

$$[p] = \pm \rho_0 c_0 [u] \quad (\text{Joukowski, 1898}).$$

Identification of three different regimes :

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# Main objectives

Identification of three different regimes :

- (I)  $M_0 \approx 1$  : fully compressible unsteady flows.
- (II)  $M_0 \ll 1$  and  $\rho_0 \approx 1 \text{ kg.m}^{-3}$  (gas,  $P_\infty = 0$ ),  $c_0 \approx 3 \times 10^2 \text{ m.s}^{-1}$ ,  
 $\rho_0 = \rho_0 c_0^2$ ,  $t_0 = l_0/u_0$  : low Mach number flows asymptotically consistent with the classical Euler incompressible system.

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- (III)  $M_0 \ll 1$  and  $\rho_0 \approx 10^3 \text{ kg.m}^{-3}$  (water,  $P_\infty \gg 1$ ),  $c_0 \approx 1.5 \times 10^3 \text{ m.s}^{-1}$ ,  
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low velocity compressible flows asymptotically consistent with the Allievi's model.

## Question :

How to derive a numerical scheme able to be accurate on the different multi-scale waves when the flow goes through the regimes (I) and (III) ?

- 1 Low-velocity flows endowed with a stiff equation of state
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# A time dynamic splitting

$$\partial_t \rho + \partial_x (\rho u) = 0,$$

$$\partial_t (\rho Y) + \partial_x (\rho Y u) = 0,$$

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- Introduce :  $\mathcal{E}_0^2(t) \in ]0, 1]$ ,  $\mathbf{U} = [\rho, \rho Y, \rho u, \rho e]^T$ .



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- Convective subsystem :  $\mathcal{C}$ . Acoustic subsystem  $\mathcal{A}$ .
- Resolution based on the  $\mathcal{C}/\mathcal{A}$  operator splitting :
  1.  $\partial_t \mathbf{U} + \mathcal{C} = \mathbf{0}$  ( $t^n \rightarrow t^{n+}$ ).
  2.  $\partial_t \mathbf{U} + \mathcal{A} = \mathbf{0}$  ( $t^{n+} \rightarrow t^{n+1}$ ).

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- Convective subsystem :  $\mathcal{C}$ . Acoustic subsystem  $\mathcal{A}$ .
- Resolution based on the  $\mathcal{C}/\mathcal{A}$  operator splitting :
  1.  $\partial_t \mathbf{U} + \mathcal{C} = \mathbf{0}$  ( $t^n \rightarrow t^{n+}$ ).
  2.  $\partial_t \mathbf{U} + \mathcal{A} = \mathbf{0}$  ( $t^{n+} \rightarrow t^{n+1}$ ).
- Time-dynamic evolution :
  - $\mathcal{E}_0^2(t) \rightarrow 1$ .

# A time dynamic splitting

$$\begin{aligned}\partial_t \rho &+ \partial_x (\rho u) &= 0 \\ \partial_t (\rho Y) &+ \partial_x (\rho Y u) &= 0 \\ \partial_t (\rho u) &+ \partial_x (\rho u^2 + p) &+ \mathbf{0} &= 0 \\ \partial_t (\rho e) &+ \underbrace{\partial_x ((\rho e + p) u)}_{\mathcal{C}=\text{Euler}} &+ \underbrace{\mathbf{0}}_{\mathcal{A}} &= 0\end{aligned}$$

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# Study of the Convective Subsystem $\mathcal{C}$

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Hyperbolicity & Eigenvalues :

- $\rho c_C^2(\rho, p) = (\partial_p \varepsilon|_\rho)^{-1} \left( \mathcal{E}_0^2 \frac{p}{\rho} - \rho \partial_p \varepsilon|_\rho \right)$  convective sound speed

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- $\forall k \in \{1, 2, 3, 4\} : \lim_{\mathcal{E}_0 \rightarrow 1} \lambda_k^C = \lambda_k^{\text{Euler}}, \lim_{\mathcal{E}_0 \rightarrow 0} \lambda_k^C = \lambda_2^{\text{Euler}} = u$

# Discretization of the convective subsystem $\mathcal{C}$

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# Discretization of the convective subsystem $\mathcal{C}$

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- A two-steps resolution :
  1. Exact solution of the Riemann problem :

$$\partial_t \mathbf{W} + \mathcal{C}^\mu = \mathbf{0}, \quad \mathbf{W}(t=0, \cdot) = \begin{cases} \mathbf{W}_L & \text{if } x < 0 \\ \mathbf{W}_R & \text{if } x > 0 \end{cases}, \quad \mathbf{W}^{\text{God}}(x/t, \mathbf{W}_R, \mathbf{W}_L).$$

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Hyperbolic relaxation system, LD fields, simple Riemann invariants.

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# Study of the acoustic Subsystem $\mathcal{A}$

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- Eigenvalues :  $\lambda_1^{\mathcal{A}} = - (1 - \mathcal{E}_0^2) c_{\mathcal{A}} < \lambda_{2,3}^{\mathcal{A}} = 0 < \lambda_4^{\mathcal{A}} = (1 - \mathcal{E}_0^2) c_{\mathcal{A}}$ .

# Discretization of the Acoustic Subsystem $\mathcal{A}$

$$\begin{aligned}\partial_t \rho &= 0, \\ \partial_t (\rho Y) &= 0, \\ \partial_t (\rho u) &+ ((1 - \mathcal{E}_0^2(t)) \partial_x p) = 0, \\ \partial_t (\rho e) &+ \underbrace{((1 - \mathcal{E}_0^2(t)) \partial_x (p u))}_{\mathcal{A}} = 0.\end{aligned}$$

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- $\mathbf{U} = [\rho, \rho Y, \rho u, \rho e]^T$ ,  $\mathbf{W} = [\mathbf{U}, \rho \Pi]$ ,  $\mathbf{S} = [\mathbf{0}, \rho (\rho(\mathbf{U}) - \Pi) / \mu]^T$ ,  
 $\tau = 1/\rho$ , Whitam's condition :  $a_{\mathcal{A}} > \rho c_{\mathcal{A}}$ .

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$$\begin{aligned}\partial_t \rho &= 0 \\ \partial_t (\rho Y) &= 0 \\ \partial_t (\rho u) + ((1 - \mathcal{E}_0^2(t)) \partial_x \Pi) &= 0 \\ \partial_t (\rho e) + ((1 - \mathcal{E}_0^2(t)) \partial_x (\Pi u)) &= 0 \\ \partial_t (\rho \Pi) + \underbrace{((1 - \mathcal{E}_0^2(t)) \partial_x (a_{\mathcal{A}}^2 u))}_{\mathcal{A}^\mu} &= \rho (\rho(\mathbf{U}) - \Pi) / \mu\end{aligned}$$

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## 1. Resolution of the homogeneous system :

- Eigenvalues :

$$\lambda_{\mathcal{A}}^1 = -((1 - \mathcal{E}_0^2(t)) a_{\mathcal{A}} \tau) < \lambda_{\mathcal{A}}^{2,3} = 0 < \lambda_{\mathcal{A}}^4 = +((1 - \mathcal{E}_0^2(t)) a_{\mathcal{A}} \tau)$$

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- Strong Riemann invariants :

$$W \equiv u - \frac{\Pi}{a_{\mathcal{A}}}, \quad R \equiv u + \frac{\Pi}{a_{\mathcal{A}}}$$



# Discretization of the Acoustic Subsystem $\mathcal{A}$

$$\partial_t \tau = 0$$

$$\partial_t Y = 0$$

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$$\partial_t (\rho e) = +((1 - \mathcal{E}_0^2(t))\partial_x (\Pi u)) = 0$$

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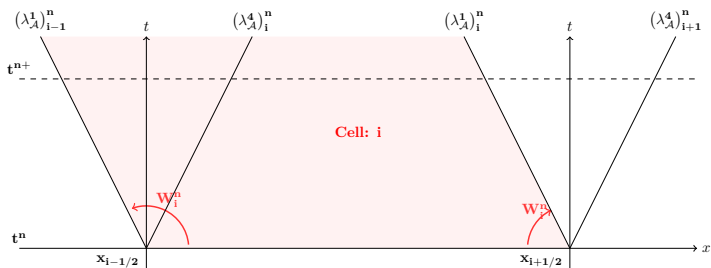
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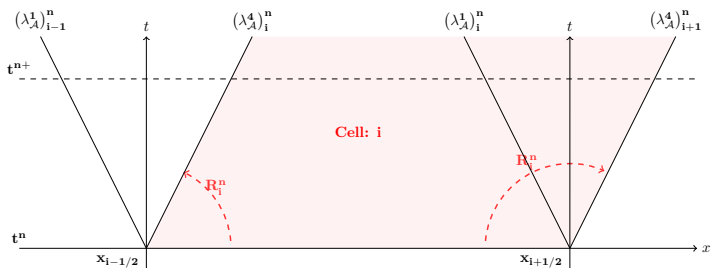
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# Discretization of the Acoustic Subsystem $\mathcal{A}$



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- Time-implicit scheme based on a strong Riemann invariants formulation (Coquel et al., 2010, Math. Comp.)

# Discretization of the Acoustic Subsystem $\mathcal{A}$

$$\tau_i^{n+} = \tau_i^n,$$

$$Y_i^{n+} = Y_i^n,$$

$$\frac{W_i^{n+} - W_i^n}{\Delta t} - \frac{(1 - (\mathcal{E}_0^n)^2) (a_{\mathcal{A}})^n \tau_i^n}{\Delta x} (W_{i+1/2}^{n+} - W_{i-1/2}^{n+}) = 0,$$

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$$\frac{(\rho e)_i^{n+} - (\rho e)_i^n}{\Delta t} + \frac{(1 - (\mathcal{E}_0^n)^2)}{\Delta x} ((\Pi u)_{i+1/2}^{n+} - (\Pi u)_{i-1/2}^{n+}) = 0.$$

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2. Instantaneous projection on the equilibrium manifold :

$$\mathcal{H}^{\text{eq}} = \{ \mathbf{W}, \text{s.t. } \Pi = \rho(\mathbf{U}) \} \quad \mathcal{P} : \mathbf{U} \rightarrow [\mathbf{U}, \rho \rho(\mathbf{U})]^T$$

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$$\rho_i^{n+1} = \rho_i^{n+}, (\rho u)_i^{n+1} = (\rho u)_i^{n+}, (\rho e)_i^{n+1} = (\rho e)_i^{n+} \Rightarrow \mathbf{U}_i^{n+1} = \mathbf{U}_i^{n+}$$

$$\Pi_i^{n+1} = \rho(\mathbf{U}_i^{n+1})$$

# Definition of the Splitting Parameter $\mathcal{E}_0(t)$

$$\begin{aligned}\partial_t \rho &+ \partial_x (\rho u) &&= 0 \\ \partial_t (\rho Y) &+ \partial_x (\rho Y u) &&= 0 \\ \partial_t (\rho u) &+ \underbrace{\partial_x (\rho u^2 + \mathcal{E}_0^2(t) p)}_C &+ \underbrace{((1 - \mathcal{E}_0^2(t)) \partial_x p)}_A &= 0 \\ \partial_t (\rho e) &+ \underbrace{\partial_x ((\rho e + \mathcal{E}_0^2(t) p) u)}_C &+ \underbrace{((1 - \mathcal{E}_0^2(t)) \partial_x (p u))}_A &= 0\end{aligned}$$

$$\mathcal{E}_0(t) = \min(M_{max}(t), 1)$$
$$M_{max}(t) = \sup_{x \in \Omega} (|u|/c)(x, t)$$

$$M_{max}(t) \geq 1$$

$$C + \mathcal{E}_0^2 A \approx C + A$$
$$(1 - \mathcal{E}_0^2) A \approx 0$$

Time-explicit Riemann solver  
Compressible waves captured

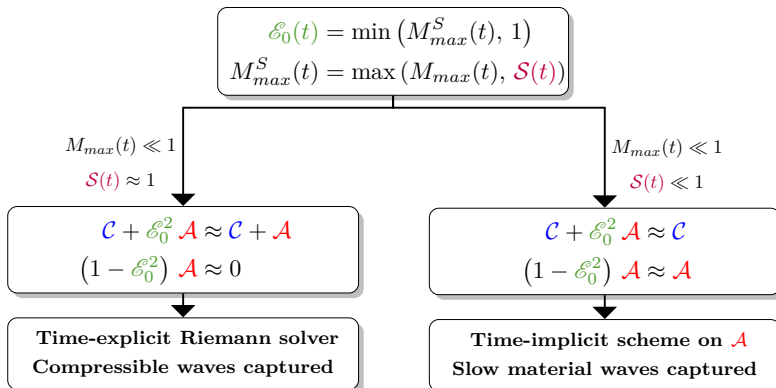
$$M_{max}(t) \ll 1$$

$$C + \mathcal{E}_0^2 A \approx C$$
$$(1 - \mathcal{E}_0^2) A \approx A$$

Time-implicit scheme on  $A$   
Slow material waves captured

# Definition of the Splitting Parameter $\mathcal{E}_0(t)$

$$\begin{aligned}\partial_t \rho &+ \partial_x (\rho u) &&= 0 \\ \partial_t (\rho Y) &+ \partial_x (\rho Y u) &&= 0 \\ \partial_t (\rho u) &+ \partial_x (\rho u^2 + \mathcal{E}_0^2(t) p) &+ ((1 - \mathcal{E}_0^2(t)) \partial_x p) &= 0 \\ \partial_t (\rho e) &+ \underbrace{\partial_x ((\rho e + \mathcal{E}_0^2(t) p) u)}_C &+ \underbrace{((1 - \mathcal{E}_0^2(t)) \partial_x (p u))}_A &= 0\end{aligned}$$



# Definition of the shock detector $\mathcal{S}(t)$

Isothermal water hammer : Joukowski's jump relation

$$[p] = \pm \rho_0 c_0 [u] \quad (\text{Joukowski, 1898})$$

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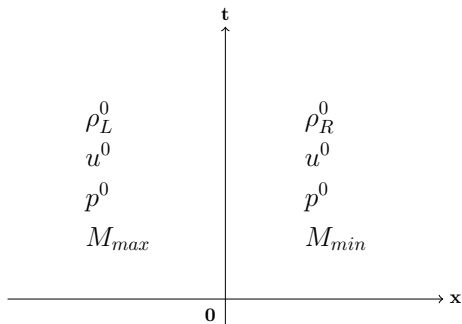
Discrete shock detector :  $\mathcal{S}(t^n)$

$$\mathcal{S}(t^n) = \sup_{i+1/2} \left( \frac{|(\sigma_s)_{i+1/2}^n|}{\max(c_{i+1}^n, c_i^n)} \right),$$

$$(\sigma_s)_{i+1/2}^n = \begin{cases} \frac{p_{i+1}^n - p_i^n}{\frac{\rho_{i+1}^n + \rho_i^n}{2} (u_{i+1}^n - u_i^n)} & \text{if } |u_{i+1}^n - u_i^n| > \epsilon^{\text{thres}} \max(|u_{i+1}^n|, |u_i^n|) \\ 0 & \text{otherwise,} \end{cases}$$

- 1 Low-velocity flows endowed with a stiff equation of state
- 2 A dynamic Implicit-Explicit scheme
- 3 Numerical results

# A Pragmatic Stability Study



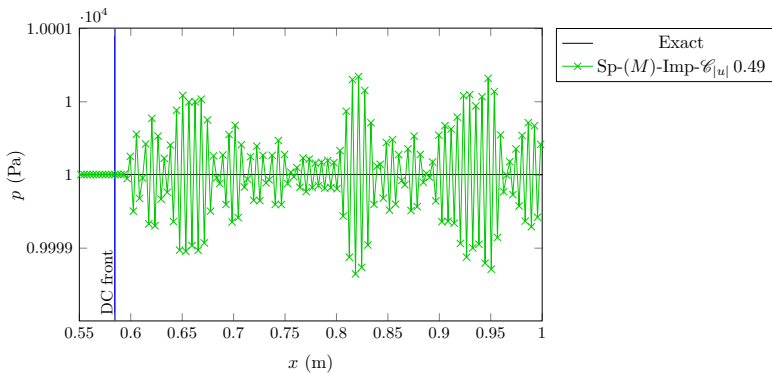
Initial conditions : single contact discontinuity

- $S(t) = 0$  imposed
- $\Delta t^n = \mathcal{C}_{|u|} \frac{\Delta x}{\max_i (|u_i^n|)}$
- Transmissive boundary conditions

- $\rho_L^0 = 1 \text{ kg.m}^{-3}$ ,  
 $\rho_R^0 = 0.125 \text{ kg.m}^{-3}$
- $p^0 = 0.1 \text{ bar}$
- Ideal gas :  $\gamma = 7/5$
- $M_{min}$  input parameter,  
 $u^0 = M_{min} c_R^0$ ,  
 $c_R^0 = \sqrt{(\gamma p^0) / \rho_R^0}$ ,  
 $M_{max} = u^0 / c_L^0 =$   
 $M_{min} \sqrt{\rho_L^0 / \rho_R^0}$

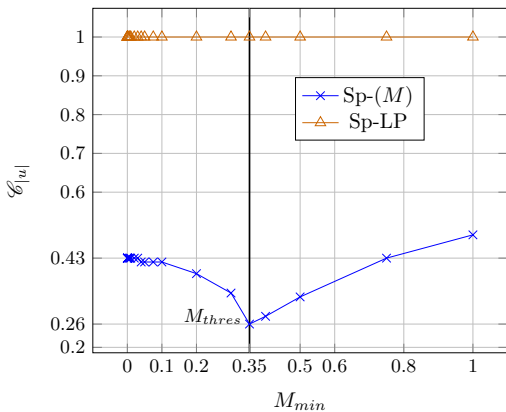


# A Pragmatic Stability Study



Pressure,  $M_{min} = 10^{-2}$ , with  $\mathbf{N}_{cells} = 10^3$ ,  $\mathcal{C}_{|u|} = 0.49$ , iteration 270,  
( $t = 2.496 \times 10^{-2}$  s)

# A Pragmatic Stability Study



Numerically measured stable Courant numbers :  $M_{min} \in [10^{-4}, 1]$

# A Pragmatic Stability Study

Tentative of explanation of the curve :

$$\mathcal{C}_C = \frac{(|u^0| + \mathcal{E}_0^n c_C^{0,R}) \Delta t}{\Delta x}, \mathcal{C}_{|u|} = \frac{|u^0| \Delta t}{\Delta x}$$

$$\text{with : } c_C^{0,R} = c_C(\rho_R^0, p^0).$$

$$\mathcal{C}_{|u|} = \left(1 + \mathcal{E}_0^n \frac{c_C^{0,R}}{|u^0|}\right)^{-1} \mathcal{C}_C = \left(1 + \frac{\mathcal{E}_0^n}{M_{\min}} \frac{c_C^{0,R}}{c^{0,R}}\right)^{-1} \mathcal{C}_C$$

$$\text{and : } \frac{c_C^{0,R}}{c^{0,R}} = \sqrt{(\mathcal{E}_0^n)^2 \frac{\gamma - 1}{\gamma} + \frac{1}{\gamma}} \in [1/\gamma, 1]$$

# A Pragmatic Stability Study

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$$\text{and : } \frac{c_C^{0,R}}{c^{0,R}} = \sqrt{(\mathcal{E}_0^n)^2 \frac{\gamma - 1}{\gamma} + \frac{1}{\gamma}} \in [1/\gamma, 1]$$

$$\underbrace{\mathcal{C}_C \approx 1}_{\text{Stability criterion}} \Rightarrow \mathcal{C}_{|u|} = \begin{cases} \left(1 + \frac{1}{M_{min}}\right)^{-1}, & \text{if : } M_{min} \geq M_{thres} = \sqrt{\rho_R^0 / \rho_L^0} \approx 0.3535 \\ \left(1 + \frac{1}{M_{thres}} \sqrt{\left(\frac{M_{min}}{M_{thres}}\right)^2 \frac{\gamma - 1}{\gamma} + \frac{1}{\gamma}}\right)^{-1}, & \text{otherwise} \end{cases}$$

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$$\text{with : } c_C^{0,R} = c_C(\rho_R^0, p^0).$$

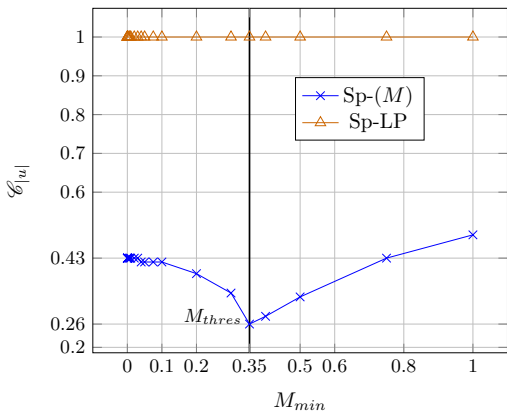
$$\mathcal{C}_{|u|} = \left(1 + \mathcal{E}_0^n \frac{c_C^{0,R}}{|u^0|}\right)^{-1} \mathcal{C}_C = \left(1 + \frac{\mathcal{E}_0^n}{M_{min}} \frac{c_C^{0,R}}{c^{0,R}}\right)^{-1} \mathcal{C}_C$$

$$\text{and : } \frac{c_C^{0,R}}{c^{0,R}} = \sqrt{(\mathcal{E}_0^n)^2 \frac{\gamma - 1}{\gamma} + \frac{1}{\gamma}} \in [1/\gamma, 1]$$

Stability criterion

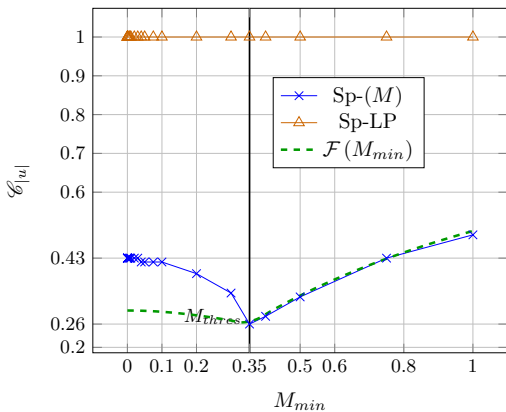
$$\underbrace{\mathcal{C}_C}_{\approx 1} \Rightarrow \mathcal{C}_{|u|} = \mathcal{F}(M_{min})$$

# A Pragmatic Stability Study



Numerically measured stable Courant numbers :  $M_{min} \in [10^{-4}, 1]$

# A Pragmatic Stability Study



Numerically measured stable Courant numbers :  $M_{min} \in [10^{-4}, 1]$

# A Double Riemann Problem with Stiff Thermodynamics

Shock tube initial conditions :  $L = 2 \text{ m}$ ,  $x_0 = 0.55 \text{ m}$ ,  $x_1 = 1.23 \text{ m}$

	Left state ( $x < x_0$ )	Intermediate state ( $x_0 < x < x_1$ )	Right state ( $x_1 < x$ )
$\rho \text{ (kg.m}^{-3}\text{)}$	$\rho_L^0 = 10^3$	$\rho_{\text{interm}}^0 = 9.98 \times 10^2$	$\rho_R^0 = 9.97 \times 10^2$
$u \text{ (m.s}^{-1}\text{)}$	$u_L^0 = 1$	$u_{\text{interm}}^0 = 1$	$u_R^0 = 1$
$p \text{ (bar)}$	$p_L^0 = 10^3$	$p_{\text{interm}}^0 = 10$	$p_R^0 = 1$
$Y$	$Y_L^0 = 0.7$	$Y_{\text{interm}}^0 = 0.2$	$Y_R^0 = 0.1$

- Thermodynamics : stiffened gas,  $\rho\varepsilon = (p + \gamma P_\infty) / (\gamma - 1)$  with  $\gamma = 7.5$  and  $P_\infty = 3 \times 10^3 \text{ bar}$ .



## Time-steps :

Convective time steps Sp-(M)-Imp :

$$\Delta t_{\mathcal{C}}^n = \mathcal{C}_{\mathcal{C}} \frac{\Delta x}{\max_{i+1/2} \left( \max \left( \left| u_i^n - \mathcal{E}_0^n (ac)_{i+1/2}^n \tau_i^n \right|, \left| u_{i+1}^n + \mathcal{E}_0^n (ac)_{i+1/2}^n \tau_{i+1}^n \right| \right) \right)}, \quad \mathcal{C}_{\mathcal{C}} = 0.9$$

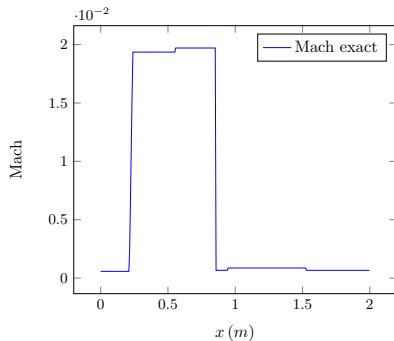
- $(a_{\mathcal{C}}^n)_{i+1/2} = K \max(\rho_i^n (c_{\mathcal{C}})^n, \rho_{i+1}^n (c_{\mathcal{C}})^n)$ ,  $K > 1$

Convective time steps LP-Imp (Chalons et al., 2016, Com. in Comp. Phys.) :

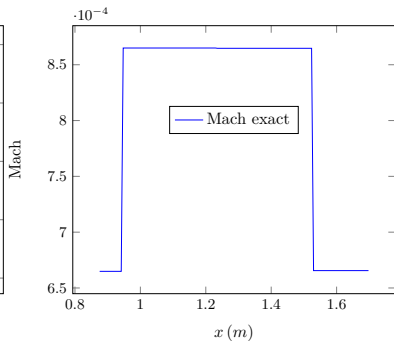
$$\Delta t_{\mathcal{C}}^n = \mathcal{C}_{\mathcal{C}} \frac{\Delta x}{\max_{i+1/2} \left( \left( (u_{\mathcal{A}}^*)_{i-1/2}^n \right)^+ - \left( (u_{\mathcal{A}}^*)_{i+1/2}^n \right)^- \right)}, \quad \mathcal{C}_{\mathcal{C}} = 0.9$$

- $(u_{\mathcal{A}}^*)_{i+1/2}^n = \frac{u_{i+1}^n + u_i^n}{2} - \frac{1}{2 a_{i+1/2}^n} (p_{i+1}^n - p_i^n)$
- $a_{i+1/2}^n = K \max(\rho_i^n c_i^n, \rho_{i+1}^n c_{i+1}^n)$ ,  $K > 1$

# A Double Riemann Problem with Stiff Thermodynamics



Mach number profile : overall area



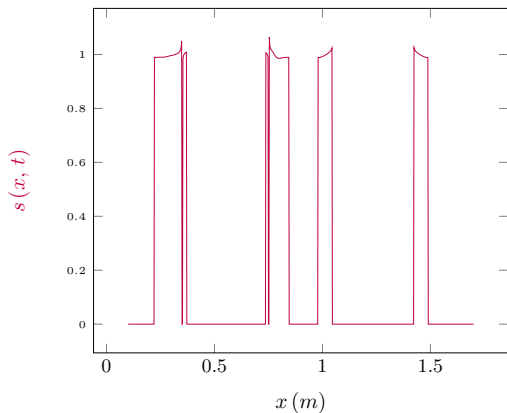
Mach number profile : low velocity area

# A Double Riemann Problem with Stiff Thermodynamics

Discrete shock detector :  $\mathcal{S}(t^n)$

$$\mathcal{S}(t^n) = \sup_{i+1/2} \left( \frac{|(\sigma_S)_{i+1/2}^n|}{\max(c_{i+1}^n, c_i^n)} \right) = \sup_{i+1/2} s_{i+1/2}^n,$$
$$(\sigma_S)_{i+1/2}^n = \begin{cases} \frac{p_{i+1}^n - p_i^n}{\frac{\rho_{i+1}^n + \rho_i^n}{2} (u_{i+1}^n - u_i^n)} & \text{if } |u_{i+1}^n - u_i^n| > \epsilon^{\text{thres}} \max(|u_{i+1}^n|, |u_i^n|) \\ 0 & \text{otherwise,} \end{cases}$$

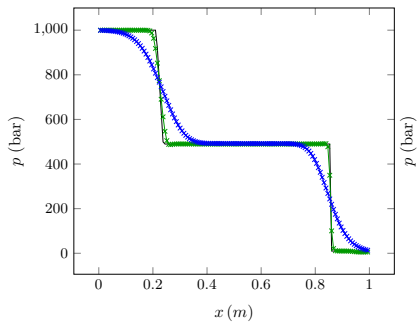
# A Double Riemann Problem with Stiff Thermodynamics



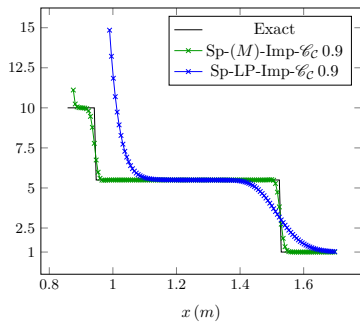
Local shock detector : overall area

Time :  $t = 1.46 \times 10^{-4}$  s

# A Double Riemann Problem with Stiff Thermodynamics

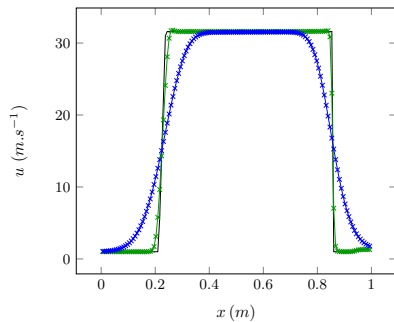


Pressure profile : high velocity area

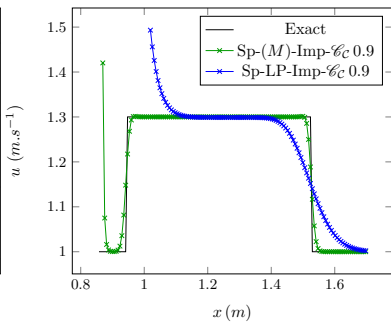


Pressure profile : low velocity area

# A Double Riemann Problem with Stiff Thermodynamics

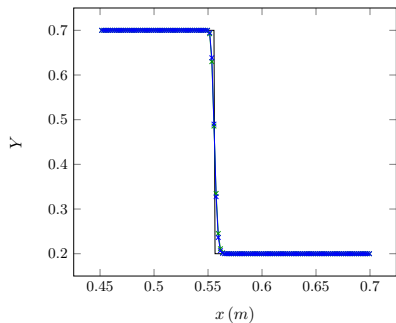


Velocity profile : high velocity area

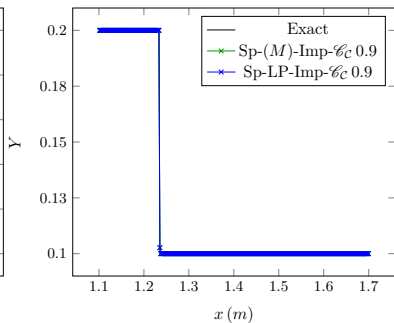


Velocity profile : low velocity area

# A Double Riemann Problem with Stiff Thermodynamics



Y profile : high velocity area



Y profile : low velocity area

	(zone 1) : $x < 0.2$ or $x > 0.8$	(zone 2) : $x \in [0.2, 0.25]$ or $x \in [0.75, 0.8]$	(zone 3) : $x \in [0.25, 0.75]$
$\rho$ ( $kg.m^{-3}$ )	$\rho^0$	$\rho^0$	$\rho^0$
$u$ ( $m.s^{-1}$ )	$u_L^0 = u^0 \times (1 - M^0/2)$	$u_R^0 = u^0 \times (1 + M^0/2)$	$u_m^0 = u^0$
$p$ (bar)	$p^0$	$p^0$	$p^0$

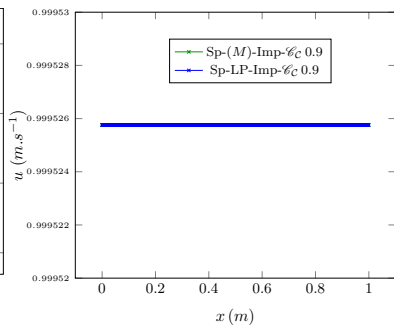
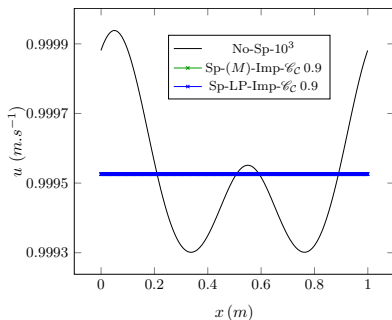
**Table:** (Dimarco et al., 2017)'s Riemann Problem : initial conditions

- $\rho^0 = 1 kg.m^{-3}$ ,  $p^0 = 1 bar$ ,  $c^0 \equiv \sqrt{p^0/\rho^0}$
- $u^0 \equiv M^0 \times c^0$ ,  $M^0$  input parameter :  $M^0 = 3.2 \times 10^{-3} \Rightarrow u^0 \approx 1 m.s^{-1}$
- Length of reference  $L^0 = 1 m$ . Time of reference  $t^0 = L^0/u^0$
- Physical time of simulation :  $T_{end} = 0.05 \times t^0$
- Ideal gas thermodynamics  $\gamma = 7/5$ ,  $\mathcal{S}(t) = 0$
- Periodic boundary conditions



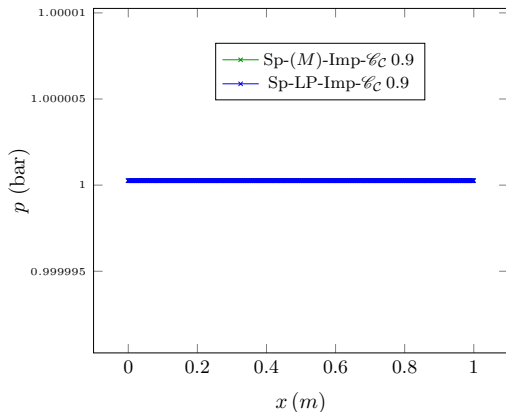
Velocity,  $M^0 = 3.2 \times 10^{-3}$

## An Asymptotic-Preserving Scheme ? (Dimarco et al., 2017, J. of Sci. Comp.)



- $u(T_{\text{end}})$  such that :

$$\int_{\Omega} \rho u(\cdot, t = 0) d\Omega = \int_{\Omega} \rho u(\cdot, t = T_{\text{end}}) d\Omega$$



Pressure profile (zoom) :  $M^0 = 3.2 \times 10^{-3}$

# Conclusion and Perspectives

## Main ideas :

- Construction of a self-adaptive IMEX scheme
- "self-adaptative" aspect due to  $\mathcal{E}_0(t)$   $\Rightarrow$  automatically select the appropriate spatial flux discretization
- $\Delta t^n \leftrightarrow |u_i^n \pm \mathcal{E}_0^n(c_c)_i^n| \Rightarrow$  automatically select the appropriate time-step

## Perspectives :

- Amelioration of the shock detector  $\mathcal{S}(t^n)$  in the ideal gas thermodynamics case
- Local formulation of the dynamic parameter :  $\mathcal{E}_0(t) \rightarrow \mathcal{E}_0(x, t)$
- Perform a proper stability analysis (linearized case, periodic BC...)

Merci de votre attention !

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