

On the Steady Motion of a Coupled System Solid-Liquid

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Preliminary Considerations

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Liquid–solid interaction (LSI) is a relatively new and fascinating branch of applied mathematics. Actually, systematic (analytical and numerical) studies started less than 15 years ago.

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Late start and current increasing interest are probably due to the following reasons:

- The intrinsic difficulties related to this type of problems. In fact, the presence of the solid (rigid or elastic) affects the flow of the liquid, and this, in turn, affects the motion of the solid, so that the problem of determining the flow characteristics is highly coupled.
- A rapidly increasing attention that, over the past decade, these questions have acquired in many fields of applied sciences, like bioengineering, animal locomotion, damage of structures, etc.

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- C1** In the case of a rigid (undeformable) body, the **interaction** between the body and the liquid is **nonlocal**: forces and torques exerted by the liquid on the body are given through **integral** quantities.

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Liquid \mathcal{L} :

$$\left. \begin{aligned} \rho (\partial_t \mathbf{v} + \mathbf{v} \cdot \nabla \mathbf{v}) &= \operatorname{div} \mathbf{T}(\mathbf{v}, p) \\ \operatorname{div} \mathbf{v} &= 0 \end{aligned} \right\} \text{in } \bigcup_{t>0} [\tilde{\mathcal{D}}(t) \times \{t\}]$$

$$\mathbf{v}(\mathbf{x}, t) = \boldsymbol{\eta} + \boldsymbol{\Omega} \times \mathbf{x}, \quad (\mathbf{x}, t) \in \bigcup_{t>0} [\partial \tilde{\mathcal{D}}(t) \times \{t\}]$$

Rigid Body \mathcal{B} :

$$m \frac{d\boldsymbol{\eta}}{dt} = \mathbf{F} - \int_{\partial \tilde{\mathcal{D}}(t)} \mathbf{T}(\mathbf{v}, p) \cdot \mathbf{N}$$

$$\frac{d(\mathbf{J} \cdot \boldsymbol{\Omega})}{dt} = \mathbf{M}_C - \int_{\partial \tilde{\mathcal{D}}(t)} (\mathbf{x} - \mathbf{x}_C) \times \mathbf{T}(\mathbf{v}, p) \cdot \mathbf{N}$$

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- C2** In the case of an elastic (deformable) body, the **deformation** of the body due to the action of the liquid becomes a **further unknown**. Moreover, the motion of the elastic body is naturally described in the **Lagrangean** formalism, while that of the liquid requires the **Eulerian** formalism.

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- Steady-state and time-periodic problems may **lack of the corresponding uniqueness property**, at **arbitrarily small** (even zero!) value of the relevant physical parameters (e.g. Reynolds number);
- Dynamics can be very rich, also at relatively small Reynolds number. **Multiple bifurcation phenomena** (steady and time-periodic) may occur.

Therefore,

- **Stability and/or Control Analysis** of the solutions is of the utmost importance, to find out which solution is “physically meaningful”.

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Therefore,

- **Stability and/or Control Analysis** of the solutions is of the utmost importance, to find out which solution is “physically meaningful”.

Most of the above phenomena remain basically **unresolved** from a mathematical viewpoint.

Body in a Viscous Liquid subject to a Constant Body Force

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Josef BEMELMANS (RWTH Aachen)

&

Mads KYED (TU Darmstadt)

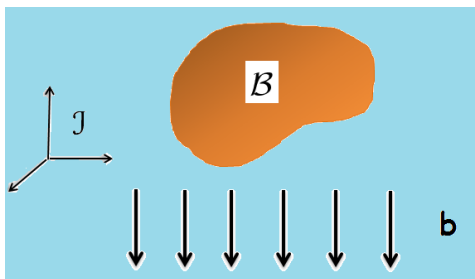
Archive Ratl Mech. Anal. (2011), Memoirs of the AMS (2012)

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Hans WEINBERGER, Proc. Symp. Pure Math. (1973)

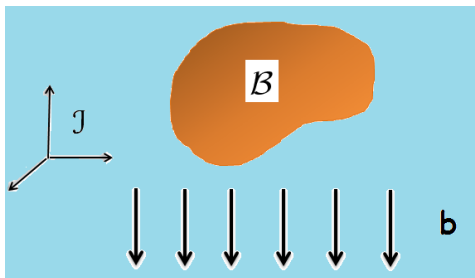
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\mathcal{B} is an **elastic (deformable) body**, that with respect to the inertial frame \mathcal{J} moves in a **viscous liquid** filling the exterior of \mathcal{B} , under the action of a **constant** (time-independent) body force \mathbf{b} .



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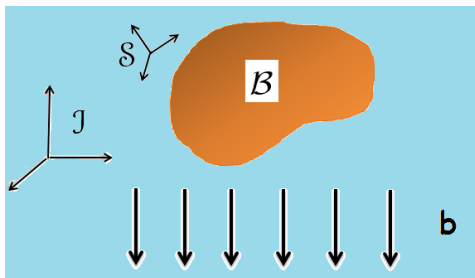
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Namely, **there exists** a frame, \mathcal{S} , with respect to which the displacement field (and so, the deformation) evaluated from a given reference configuration is **time-independent**.

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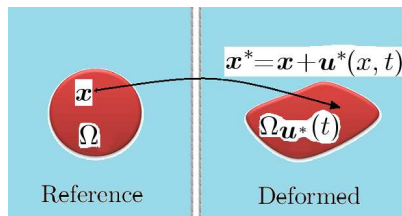
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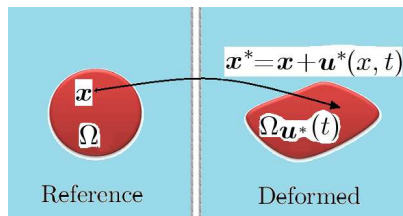


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ρ_E is the **constant density** (in the reference configuration),
 $\boldsymbol{\sigma}$ is the (first) **Piola-Kirchhoff tensor**.

The Solid-Liquid Problem in the Frame \mathcal{J}

To fix the ideas, we will consider **St.-Venant–Kirchhoff elastic bodies**, for which

$$\boldsymbol{\sigma}(\mathbf{u}^*) = (\mathbf{I} + \nabla \mathbf{u}^*)(\lambda_E \text{Tr} \mathbf{E}(\mathbf{u}^*) \mathbf{I} + 2\mu_E \mathbf{E}(\mathbf{u}^*))$$

$$\mathbf{E}(\mathbf{u}^*) = \frac{1}{2} \left(\nabla \mathbf{u}^* + \nabla \mathbf{u}^{*\top} + \nabla \mathbf{u}^{*\top} \nabla \mathbf{u}^* \right)$$

\mathbf{I} = identity matrix, $\mu_E > 0$ and $\lambda_E > -\frac{2}{3}\mu_E$ are the **Lame constants**.

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The deformed configuration of the body is:

$$\Omega_{\mathbf{u}^*}(t) = \{\mathbf{x}^* \in \mathbb{R}^3 : \mathbf{x}^* = \mathbf{x} + \mathbf{u}^*(\mathbf{x}, t), \mathbf{x} \in \overline{\Omega}\}, \quad t > 0,$$

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The liquid occupies the region, $\mathcal{E} = \mathcal{E}(t)$, exterior to $\Omega_{\mathbf{u}^*}(t)$, that is,

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We thus have

$$\left. \begin{aligned} \rho(\partial_t \mathbf{v}^* + (\nabla \mathbf{v}^*)\mathbf{v}^*) &= \mu \Delta \mathbf{v}^* - \nabla p^* \\ \operatorname{div} \mathbf{v}^* &= 0 \end{aligned} \right\} \text{ in } \cup_{t>0} [\mathcal{E}(t) \times \{t\}].$$

\mathbf{v}^* is the velocity, p^* is the pressure,
 ρ is the density, μ is the shear viscosity coefficient

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Conditions at the Solid-Liquid Interface $\partial\Omega_{\mathbf{u}^*}(t)$

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For sufficiently “regular” $\mathbf{u}^*(\cdot, t)$ ($|\nabla\mathbf{u}^*(\cdot, t)| < 1$), we have

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Continuity of the Stress:

$$\mathbf{T}_L \cdot \mathbf{n} = \mathbf{T}_E \cdot \mathbf{n} \quad \text{at } \cup_{t>0} [\partial\Omega_{\mathbf{u}^*}(t) \times \{t\}],$$

where

\mathbf{T}_E is the Cauchy stress tensor of the elastic body

\mathbf{T}_L is the Cauchy stress tensor of the liquid

\mathbf{n} is the outer unit normal to $\partial\Omega_{\mathbf{u}^*}(t)$.

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Let $\boldsymbol{\omega}$ be the **unknown constant** angular velocity of the frame \mathcal{S} with respect to the inertial frame \mathcal{J} , and set

$$\hat{\boldsymbol{\omega}} = \begin{pmatrix} 0 & -\omega_3 & \omega_2 \\ \omega_3 & 0 & -\omega_1 \\ -\omega_2 & \omega_1 & 0 \end{pmatrix}.$$

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If $\mathbf{x}^* = \mathbf{x} + \mathbf{u}^*(\mathbf{x}, t)$, we make the following change of variables

$$\mathbf{y} = e^{-\widehat{\boldsymbol{\omega}}t} \cdot (\mathbf{x}^* - \mathbf{x}_c^*), \quad \mathbf{x} \in \Omega; \quad e^{-\widehat{\boldsymbol{\omega}}t} \in SO(3), \quad t \geq 0.$$

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Thus, **with respect to \mathcal{S}** , the **displacement field** is given by:

$$\mathbf{u}(\mathbf{x}, t) = \mathbf{y} - \mathbf{x}, \quad \mathbf{x} \in \Omega,$$

and the **velocity of the center of mass**:

$$\boldsymbol{\xi} = e^{-\widehat{\boldsymbol{\omega}}t} \cdot \partial_t \mathbf{x}_c^*.$$

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Equations of Motion for the Elastic Body

$$\begin{aligned} & \rho_E [\partial_t^2 \mathbf{u} + \boldsymbol{\omega} \times (\boldsymbol{\omega} \times (\mathbf{x} + \mathbf{u})) + 2\boldsymbol{\omega} \times \partial_t \mathbf{u}] \\ & + \rho_E (\boldsymbol{\omega} \times \boldsymbol{\xi} + \partial_t \boldsymbol{\xi}) = \operatorname{div} \boldsymbol{\sigma}(\mathbf{u}) + \rho_E e^{-\hat{\boldsymbol{\omega}} t} \cdot \mathbf{b}, \quad \text{in } \Omega \times (0, \infty). \end{aligned}$$

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The **direction** of the vector \mathbf{b} becomes a **further unknown**.

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where

$\boldsymbol{\omega}$, $\boldsymbol{\xi}$, \mathbf{b} and $\mathbf{u} = \mathbf{u}(x)$, $x \in \Omega$, are **unknown**,

and

$|\mathbf{b}| = |\mathbf{b}|$ is **given**.

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Set

$$\mathbf{v}(\cdot, t) = e^{-\widehat{\boldsymbol{\omega}}t} \cdot \mathbf{v}^*(e^{\widehat{\boldsymbol{\omega}}t} \cdot + \mathbf{x}_c^*, t), \quad p(\cdot, t) = e^{-\widehat{\boldsymbol{\omega}}t} p^*(e^{\widehat{\boldsymbol{\omega}}t} \cdot + \mathbf{x}_c^*, t)$$

and require that (\mathbf{v}, p) is **steady**.

The Solid-Liquid Problem in the Frame \mathcal{S}

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$$\left. \begin{aligned} \rho[\nabla \mathbf{v}(\mathbf{v} - (\boldsymbol{\omega} \times \mathbf{y} + \boldsymbol{\xi})) + \boldsymbol{\omega} \times \mathbf{v}] &= \mu \Delta \mathbf{v} - \nabla p \\ \operatorname{div} \mathbf{v} &= 0 \end{aligned} \right\} \text{ in } \mathcal{Y}$$

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No-slip **boundary condition** becomes

$$\mathbf{v} = \boldsymbol{\xi} + \boldsymbol{\omega} \times \mathbf{y} \quad \text{at } \partial \mathcal{Y}.$$

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The **final step** is to rewrite the liquid equations in the exterior of the **reference** (undeformed) configuration, $\mathbb{R}^3 - \Omega$.

This can be done if \mathbf{u} is “sufficiently regular”.

The Solid-Liquid Problem in the Frame \mathcal{S}

Lemma Let $\mathbf{u} \in W^{2,q}(\Omega)$, $q > 3$, with

$$\|\mathbf{u}\|_{W^{2,q}(\Omega)} \leq M \quad \text{“sufficiently small”}$$

Then there is a C^1 -diffeomorphism, $\chi_{\mathbf{u}}$, from \mathbb{R}^3 onto itself satisfying the following properties.

- (i) $\chi_{\mathbf{u}}(\mathbf{x}) = \mathbf{x} + \mathbf{u}(\mathbf{x})$ for all $\mathbf{x} \in \overline{\Omega}$;
- (ii) $\chi_{\mathbf{u}}(\mathbf{x}) = \mathbf{x}$, for all \mathbf{x} with $|\mathbf{x}| \geq R$, some $R > 0$.

In particular, $\chi_{\mathbf{u}}$ is a C^1 -diffeomorphism from $\mathbb{R}^3 - \Omega$ onto \mathcal{Y} .

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Using the diffeomorphism $\chi_{\mathbf{u}}$ we can rewrite the liquid equations in $\mathbb{R}^3 - \Omega$ and end up with the following **complete set of equations**

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where

$\mathbf{T}^{(\mathbf{u})}(\mathbf{v}, p)$ = Transformed Liquid Cauchy Tensor

$$J_{\mathbf{u}} := \det(\operatorname{grad} \chi_{\mathbf{u}}), \quad \Phi_{\mathbf{u}} := J_{\mathbf{u}} (\operatorname{grad} \chi_{\mathbf{u}})^{-1}$$

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Problem. Given $\rho_E, \rho, \mu, \lambda_E, \mu_E, \mathbf{b}$ and a reference configuration Ω for \mathcal{B} , find $\mathbf{u}, \mathbf{v}, p, \boldsymbol{\xi}, \boldsymbol{\omega}$ and \mathbf{b} satisfying above conditions.

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Therefore, for the **existence**, we have to find $\lambda \in \mathbb{R}$ in such a way that (1)–(2) has a solution with a normalized $\mathbf{b} \neq \mathbf{0}$ (for example, $\mathbf{b} \in S^2$).

Sketch of the Strategy of Proof and Main Results

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The main idea develops according to the following steps:

- Linearize the problem suitably
- Find a (suitable) solution to the linearized problem
- Iterate around this solution
- Find a solution to the original problem (for small data)

Sketch of the Strategy of Proof and Main Results

Linearization

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$$\operatorname{div} \boldsymbol{\sigma}^L(\mathbf{u}_0) \equiv 2\nu \nabla(\operatorname{div} \mathbf{u}_0) + 2(1 - 2\nu) \Delta \mathbf{u}_0 = -\mathcal{T} \mathbf{b}_0 \quad \text{in } \Omega,$$

$$\nu := \frac{\mu_E}{\lambda_E + \mu_E}$$

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Compatibility Conditions:

$$-\mathcal{T} |\Omega| \mathbf{b} = \int_{\partial\Omega} \mathbf{T}(\mathbf{v}_0, p_0) \cdot \mathbf{n}, \quad \int_{\partial\Omega} \mathbf{x} \times (\mathbf{T}(\mathbf{v}_0, p_0) \cdot \mathbf{n}) = \mathbf{0}.$$

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Eigenvalue Problem:

$$\begin{aligned}\mathbb{A} \cdot \mathbf{b}_0 &= \lambda_0 \mathbf{b}_0 \\ \boldsymbol{\xi}_0 &= \mathbf{F}(\mathbf{b}_0, \lambda_0)\end{aligned}\tag{4}$$

where \mathbb{A} is a real, 3×3 matrix depending **only** on the “shape” of Ω .

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The iterative scheme to solve the original problem, works on condition that **the “shape” of Ω** is such that the eigenvalue problem

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has at least one eigenvalue **of algebraic multiplicity 1**.

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One thus shows that **linearized** problem (3) has **at least one** solution. In fact, depending on the “shape” of Ω , it may have even an **infinite number** of solutions.

The iterative scheme to solve the original problem, works on condition that **the “shape” of Ω** is such that the eigenvalue problem

$$\mathbb{A} \cdot \mathbf{b}_0 = \lambda_0 \mathbf{b}_0 \quad (4)$$

has at least one eigenvalue **of algebraic multiplicity 1**.

Theorem 1

Suppose the reference configuration Ω is such that (4) has at least one simple eigenvalue λ_0 . Then, there is $\epsilon_0 > 0$ such that if

$$\rho_E D_0 |\mathbf{b}| \leq \epsilon_0 (\mu_E + \lambda_E)$$

the nonlinear problem has at least one solution.

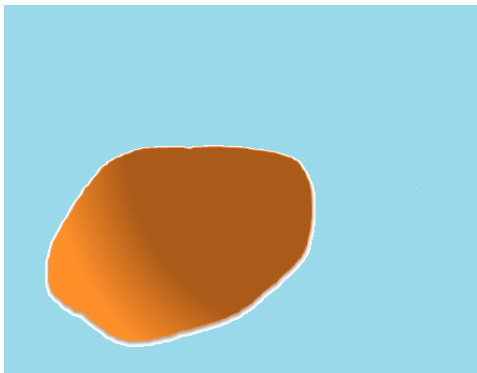
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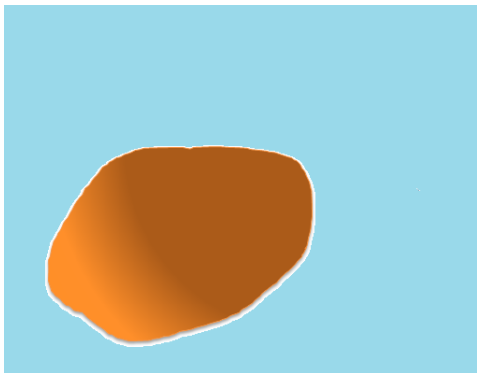
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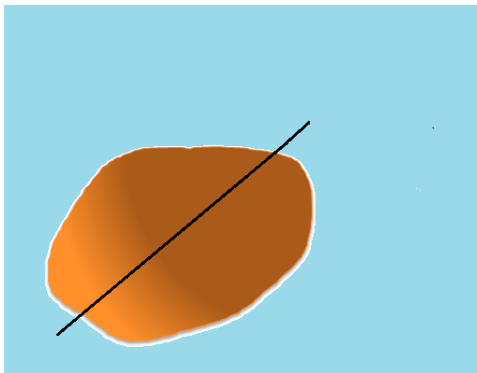


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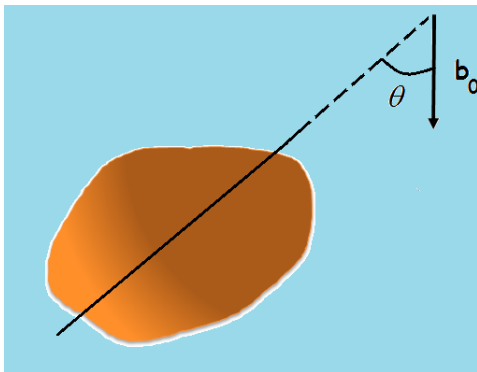


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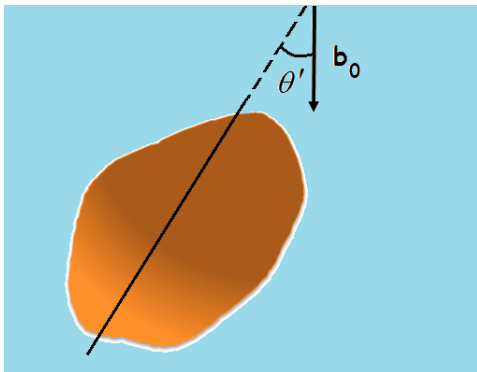


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Theorem 2

Suppose the reference configuration Ω is symmetric. Then, there is $\epsilon_0 > 0$ such that if

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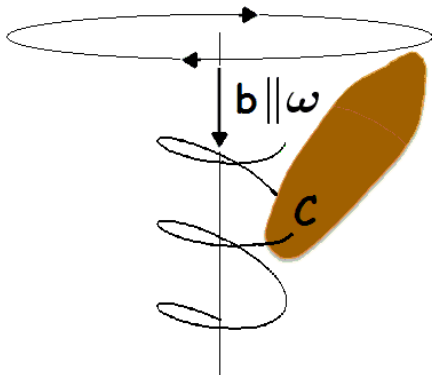
OPEN QUESTION: Do steady-state regimes exist for reference configurations of arbitrary shape?

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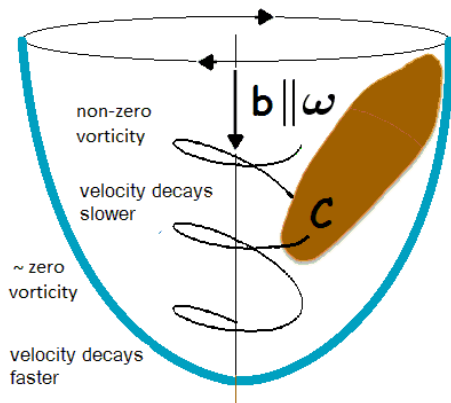
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Questions 2–4 are **open** also in the case of a **rigid** body.